GV 435 .H68 Copy 1

11STI-

THE

ANTHROPOMETRIC TABLES

AMHERST COLLEGE.

1892.



THE

* RESULTS OF ANTHROPOMETRY.*

AS DERIVED FROM THE MEASUREMENTS OF THE STUDENTS

IN AMHERST COLLEGE.

A PAPER PRESENTED TO THE AMERICAN ASSOCIATION FOR THE AD-VANCEMENT OF PHYSICAL EDUCATION AT THEIR ANNUAL MEETING IN PHILADELPHIA, APRIL, 1892.

= Hitchcock, Edward >

AMHERST, MASS.: Press of Carpenter & Morehouse, 1892.

C+1435

Dy Eventier. 188'06

PHYSICAL MEASUREMENTS AS AFFORD-ING A BASIS FOR THE DETERMINA-TION OF THE IDEAL MAN.

More than a century ago, Sir Joshua Reynolds in England used this language:

"From reiterated experience and a close comparison of the objects of nature, the artist becomes possessed of a central form from which every deviation is deformity. * * * * And as there is one general form which belongs to the human kind at large, so in each of these classes there is one common idea and central form which is the abstract of the various individual forms belonging to that class. I must add further, that though the most perfect forms of each of the general divisions of the human figure are ideal, and superior to any individual forms of that class, yet the highest perfection of the human figure is not to be found in any one of them. It is not in the Hercules, nor in the Gladiator, nor in the Apollo; but in that form which is taken from them all, and which partakes of the activity of the Gladiator, of the delicacy of the Apollo, and the muscular strength of the Hercules."

The object of this article is not to exhibit on paper or in figures the ideal human form, but believing there is an ideal form as conceived in the Divine mind, and that this ideal is by no means as yet present to us in the bodies of our young men; but to show that the studies here presented may give us some glimpses of this ideal, and how we may approximate to it. Or, perhaps it is better to say that these studies show us what is the best human form and proportion as it actually exists to-day, and then from the special and peculiar excellencies as brought out in these researches, we can set ourselves to work to see if we cannot elevate the average to a higher ideal.

But firstly let us bring up a little past history of the study of the human form in ideal.

The Sanscrit manuscript written in the early Christian centuries is the oldest literature on this subject. It is called the Silpi Sastri, and with great exactness and precision divides the human body into nine portions, and 480 parts.

The hair,	15
The face,	55
The neck,	25
The chest,	55
From the chest to the navel,	55
Thence to the pubes,	53
" knee,	90
The knee itself,	30
The leg and foot,	102
	480

And by a most "occult" administration of a tangle of squares, circles and triangles it was "demonstrated" in this manuscript what the perfect human form might be expected to resemble.

A Greek sculptor Polykleitus about 400 years B. C. has left a treatise called the "canon" on human proportions. This was illustrated by a marble statue called Doryphorus, or Spear Bearer, which was said to have been of "perfect proportions." But the model has disappeared.

Phidias, still later, employed twenty models, borrowing from each of them the most beautiful parts "permitting him to arrange them with all the necessary strength and dignity."

And other schemes have been devised, and have perished, by other lesser lights among artists ancient and modern, endeavoring to tell us what is the perfect or ideal human form.

But near the beginning of the present century, as scientific methods have come to the front to confirm or overthrow theory as it may be true or false, the artistic conception has been asked to wait a little while, until patient, plodding, scientific investigation shall show us what we now have on hand to enable us to try and construct the artistic ideal.

And the first investigator in this field of research is no less a man than Baron L. A. G. Quetelet of Belgium, in the prime of his activities from 1850 to 1870. His work which we find under the different captions of "proportions," "superficial extent," "development," "measure of the different faculties" and "theory of probabilities of the human body" he most carefully carried out by observation, experiment, and use of the doctrine of means and averages over an immense field of investigation. And to Baron Quetelet we must give the title of the Father of Anthropometry.

Since the year 1884, the American Association for the Advancement of Physical Education has received, and there have been read at its annual meetings many papers on anthropometry and its kindred subjects. It has also adopted a definite method of ascertaining the proportions of the human body mainly as derived from measurements made in colleges, schools and the Y. M. C. associations.

Working in the very close direction of the method adopted by this association, the Department of Physical Education in Amherst College has been making a prolonged and careful study of the physical statistics of all of the nearly 3000 students who have been connected with this Institution during the last thirty years. The results of study have been carefully preserved, collected and tabulated in several different ways, and the most important of them are appended to this paper. It has not, however, been the design in it all, to labor according to any preconceived theory or model, but merely to gather together the facts, and then find out the law or method which they seem to outline or foreshadow.

This large mass of measurements has been looked at, arranged and tabulated in the following different ways.

The first one is in the common method of taking the Average of each item of all the students measured. This means, adding together the measures of each student, and then dividing the amount by the total number of students observed. This is to be found under the table of the Average Student.

As twenty-one years is considered by common law to be the date of arriving at full manhood, the measurements of those who were between Twenty-one and Twenty-two Years of Age are arranged and exhibited under the table The Student Twenty-one Years Old.

For the sake of further unfolding the subject, these measurements have been arranged and tabulated according to the doctrine of means, or, of mean proportions. The method of securing this, is, to arrange all the items in groups with a common difference, from the least to the greatest, when we readily find the group with the largest number, which represents the mean number of the whole. This is found under table 3, or the one of the Student of mean proportions.

Another way of illustrating these results is the grouping of all the items by the Ages of the Individuals. The ages as studied here have been from sixteen to twenty-six. This is the Table of Ages.

The Percentile Method is another way of expressing the results of these measurements. This method is analogous to that of the

"means." The items here are all arranged in order from the greatest to the least, when five per cent. are counted off for the first division, ten more for the second, and so on down to fifty per cent., which corresponds very closely with the "average," or "mean," as already described. These five divisions indicate a measure above the fifty per cent. Then another division of ten per cent. indicates forty per cent. below the fifty per cent. division; and another ten, per cent, thirty more below, and so on to the minimum of five per cent.

The last table is that with STATURE for a basis of comparison. Here all the items are grouped together under the differing body heights, from the lowest to the highest with the variation of one centimeter, or about half an inch in each group. For instance, taking the lowest group measuring 1600 m. m. or 63 inches, all men of this height—1600 to 1609— are tabulated together and each of the fifty-four items averaged to secure the standard of measurements for men of the heighth of 1600 m. m., or 63 inches. Then the other heights, 1610, 1620 and so on up to 1830 m. m., or 72 inches, are tabulated in the same manner. This is the table represented By Heights.

Thus are brought side by side six different ways of studying the anthropometric results obtained from the students of Amherst College. And it certainly is both instructive and interesting to see the close relation of results in these different methods, and very likely if we feel that we must adopt one of these several methods, we shall have to be on our guard lest we should need the advice of the countryman to the traveler who inquired which was the best of three roads before them, "all of them lead you there, but whichever one you take before you get there you'll wish you had taken the other."

For, without doubt, age, weight, stature and per cent. are each important factors in this problem, when we are to treat it in a cosmopolitan manner. But for educational and developmental study, where so much of the need of physical training now lies, for the training, strengthening and developing weak and poorly developed bodies, the Standard of Stature seems the safest and surest to work from. The painter and sculptor certainly makes his dimensions of size according to the height of the subject he is placing on canvas or in marble. There are certain limits to the outline of the tall person which he would not give to a shorter figure, even if the age were exactly the same. He would not add the encumbrance of fat to the figure short and chubby, even though the theory was ever so strong that just so much adipose must be there all the same, no matter

what the lengths of the bone so warmly covered up might be. And it seems rational to suppose that the capacity and size of the vital organs, and the strength of the muscles, to move the longer or shorter levers will be proportioned to the length of trunk and limb, rather than to the mere weight of the tissues. Also the facts are established, beyond doubt, long ago, that the size of the lungs and some other vital organs, depends in each individual case upon the bodily stature, so many additional cubic inches of lung capacity for each inch of stature. And as strength of muscle depends on the number rather than the length of its fibers, we shall see that the long arm or leg needs a thicker muscle to move it than does a shorter one. Hence the trunk, arm or leg of the person a little longer than another of exactly the same age or weight, would require a little longer girth measure, to endue it with the strength proportioned to the size.

It will not, however, be right to dismiss this subject without presenting to this association the opinion of Mr. Charles Roberts, the foremost authority on anthropometry in Great Britain to-day. In treating of the subject in "index columns, age columns and result columns," he sums up the whole by saying, "the total height being the most characteristic and important measurement of the body, the arrangement of the table of heights has been made the model for all the rest."

In concluding, it seems safe to say, that the examination of the tables constructed on Bodily Stature as a datum give strong support to the idea that this element is the determining basis for an anthropometric standard whether of the ideal man, or for rational deductions and prescriptions for a better or more normal rate and quality of bodily growth.

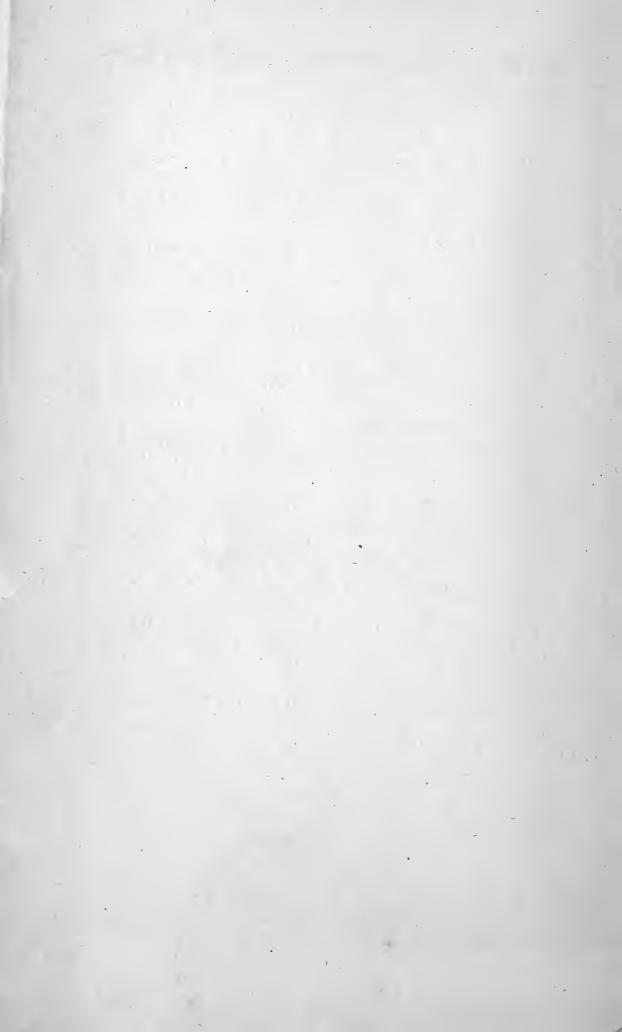
It is a pleasure and privilege to say that the preparation and printing of these tables, and the offer of a copy to each member of this association is made possible by the endowment of a "contingent fund" for anthropometric, and its kindred work in Amherst College by Dr. Rufus P. Lincoln in New York.



stridy of the Str

The o're to guess consequention that as kilomans and liters; the

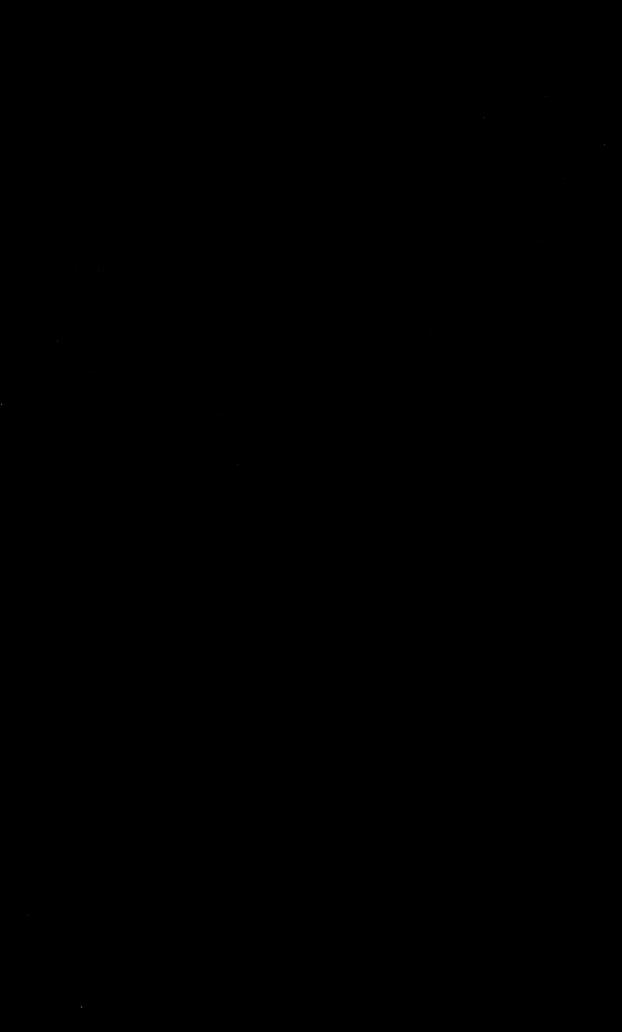
	entino
BY AGE.	Frein Dass Frein
	CABLE OF THE AVIERA CHIEF
	2. TABLE OF THE STUDENT OF THE STUDE
	8. TABLE OF THE STUDENT OF M
	-i, TABLE OF 80 PER CENT. M
	S. TARLE DE ACCESSION AND AN AN AND AND AND AND AND AND AND
16 year	
17 "	
18 "	1
19 "	or at The Mis old 1965 steining has not aid to the de-
20 ''	्राति है के स्थाप के लिए हैं के स्थाप के लिए हैं के स्थाप के कि स्थाप के स्थाप के स्थाप के स्थाप के स्थाप के स
21 "	THE ONLY THE REPORTS AND THE THE REPORT OF THE
22 "	TO THE REAL PROPERTY OF THE STEEL STEEL THE
23 "	
24 ''	The sist and the particular one one of the are are are able to a
25 ''	FOUNDED TO THE TOTAL PROPERTY OF THE COMMENT OF THE STATE OF THE PROPERTY OF THE COMMENT OF THE STATE OF THE PROPERTY OF THE COMMENT OF THE STATE OF
26 "	रक्षा कार्यात व्यक्ति विश्वति विश्वति विश्वति । स्वति विश्वति । स्वति । स्वति । स्वति । स्वति । स्वति । स्वति ।



Anthropometric Study of the Students of Amherst College.

The black figures represent millimeters, kilograms and liters: the red, inches, pounds and cubic inches.

	1			(_														-, 20																			1	
	T	T	11	EIGHTS.													GIR	THS.					_										16	BR	EADI	us.				Fr	ENGT	HS,		2	s	TREN	GTHS			G.	Ī	ED
BY AGE.	WEIGHT.	Body.	Starnum.	Navel.	Knee.	sitting.	Head.	Neck.	Chest Repose.	Chest Full.	Belly.	Hips. •	Right Thigb.	Left Thigh.	Right Knee.	Left Knee.	Right Calf.	Left Calf.	Right Instep.	Left Instep.	Upper Right Arm Contract	Upper Right	Upper Left	Right E.bow.	Left Elbow.	Right Forentm	Left Forearm.	Discht Weder	right whist		Head.	Neck.	Shoulder.	Nipples.	Waist.	Right Shoulder	Left Shoulder Elbow.	Rigbt Elbow Tip.	Left Elbow Tip.	Right Foot.	Left Foot.	Arms. Horizontal	Length	Back.	Dip.	Pull.	Legs.	Right Forearm	Lert Forearm. Total.	CAPACITY OF LUNGS	PILOSITY.	NUMBER OF MEN MEASURE)
			-1-2		4														1.												ST																					
	61.2	1725	5 1410 10 55.5 4	030 860 0.5 88.9	476 18.7	903	572	349	880	927 36.5	724 28.5	893 35.1	517 20.3	512 20.2	361 14.2	359 14.1	359 14.1	349 13.7	$\begin{array}{c c} 245 \\ 9.6 \end{array}$	242 9,5	295 11.6	257	$\begin{vmatrix} 25 \\ 1 \end{vmatrix}$	8 25 0 9.	1 24 8 9.	7 26 7 10.	7 26 5 10	$\begin{bmatrix} 1 \\ 3 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$	66 1 5,5 0	65	[55] [6,]	108 4	30 1	198 2 7.8 5	50 3:).8 12	28 378 .7 14.	3 371 7 14.6	461 18.1	$\begin{bmatrix} 459 \\ 18.1 \end{bmatrix}$	$\frac{260}{10.2}$	259 1 10.2 7	780 1 0.1 6	732 1 8.2 3.	.5 137 81 802	6	9	166 365	41 8 90 8	88	3.77	li	798
-																																		OLI																		
	63.1	11726 67.9	1407 10 55.3 40	25 864 0.4 34.0	477 18.7)03 5.5	572 22.5	356 14.0	892 85.1	933	725 28.5	898 35.8	521 20.5	519 20.4	$359 \\ 14.1$	358 14.1	350 13,8	348 13.7	244 9.6	9.6	301 11.8	1 26- 8 10.	4 25 3 10	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	3 24 .0 9	9 26 .8 10	6 2.5 .5 10	59 1	66 1 6.5 6	65 1	55 1	09 4 1.3 10	31 2 5.9 7	200 2 7.9 10	56 35 .1 12	374 .9 14.	374 7 14.7	462 18.1	459 18.1	261 10.3	260 1 10.2	794 1 70.6 6	738 1 8.4 3	.4 140 .10 32	7	10	172 378	41 8 90 8	39 86	4.23 258		32
																3	ΤА	ВI	Æ	OF	гΤ	'HI	E 5	тт	IDE	ENT	Γ	F	M	₹.A.	N F	2R)P	OR	TIC	NS																
	164.0	1720 67.7	1410 10 55.5 40	23 860 .3 33.9	480 3 18.9 3	5.8	570	350 3.8	880	925 36.4	720 28.3	890 35.0	515 20.3	510 20.1	360 14.2	360 14.2	359 14.1	350 13.8	240 9.4	240 9.4	295	5 26 6 10	0 25 2 9.	0 25 8 9.	0 25 8 9.	0 20 8 10	6 20 6 10	60 1	65 1 6,5 6	65 1 .5 6	54 1 3.1 4	10 4 .8 10	30 2 i.9 7	00 2	50 32 .8 12.	0 370 6 14.0	370 3 14.6	460 18.1	460 18.1	260 10.2	260 [0.2]	177 0 1 39.7 6	$730 1 \\ 8.1 2$.2 15 $.64 33$	0 4	10	175 386	40 88	87 82	3.90 238		208
		-																																ENT																		_
	61.6	1724 67.8	1410 10 55.5 40	29 864 .5 34.0	476 S	05 5.6 2	569 2.4	351 3 3.8 3	885 4.8	925 36.4	730	893 35.1	514 20.2	510 20.1	359 14.2	359 11-2	347	845 13.6	242 9.5	241 9.5	295 11.0	5 259 10.	2 9	2 25	0 24 .8 9	7 26 .7 10	2 25	56 1	65 1 6.5 6	68 1	53 1	08 4	33 1	96 2	58 35	25 375 .8 14.	3 371	461 18.1	459 18.1	260 10.2	260	1789 1 70.4 (739 1 8,4 3	.4 13 .10 30	6	9	169 373	39 86 :	37 453 82	3 3.89 237		22;
	-		· ·								-										-					_E																										
6 yea	100 (4- 4-	1415 10	0 24 1	10 0 9	5 0 1	19 1	2 5 5	12 8 51	5 4 5	7.7 %	23 6 1	19.8	19 (C)	14 0	14.41	3.5 1	3.3	9.5	9.5	11.0	1. 9.3	s 9.	4 ' 9.	6 9.	4 10.	(1 9)	.8 (1.5 C	5.41 (6.1 - 4	1.2 11	i.4 i	7.4 :	-7 - 12	.6.14.	7 114.6	18.3	18.2	10.3 .	10.3 ± 7	0.1.68	$5.2 \pm 2.$.31 136 9 280	5		151 333	77	75	3.91 239		
**	12000 0	n- n	1411 10 55.5 40 1419 10	7 010	10000	5 t 1	200 1	0 5 0	0 - 0	10 9	0 1 2	2.1 7	10 0	19 8	1.1 1	14 1 1	3 1 1	3 3	9.7	9.5	111 1	19.7	(9	5 9	6 9	5 10.	0 - 9.	.7 (i.5 - 6	5.41 (6.01:	1.2 110	3.8 °	7.5 1 1	0.7 ± 12	.7 14.	6 14.5	18.1	118.01	10.3	10.3 7	0.1168	8.4 [3.	0 (27)	5	8	150 331 158	82	75	3 4.01 245 3 4.11		
	134.2	68.2	55.9 40 1413 10	.9 34.3 30 867	18.9 8	5.6 2	2,2 1	3.7 3 354 8	4.1 3 82 9	6.1 2	8.5 £	898 ±	$\frac{20.2}{514}$	19.9	359	360	$\frac{3.5}{1}$	5.5 345	9.6	9.6 244	296	258	251	8 9.	8 9. 3 240	6 26	1 25	(4 10	66 16	i.4 i4 1	6.1 + 3	E.2 III	5.9	1.6 1 5	1.9 112	.7 14.	8 14.7	18.3	18.33	10.3	10.8 7	0.5:68	5.8 [3.	1 20s 43 145	i .	10	348 167	101	79 37 448	$\frac{251}{4.11}$	2.36	
) *:	135.4 63 00	$\frac{68.2}{1731}$	55.6 40	37 869	18.8	5.5	2.3	3.9 3	4.7 3	6.5 2	8.7 8	35.3 S	$\frac{20.2}{515}$	20.1	360	14.2 I 360 I	3.7 1: 349 3	3.6	9.7	9.6	11.6	10. 262	250	9 (). i 251	7 9. 2 247	6 [10, 7 263	$\frac{3!10}{3!25}$	7 10	5.5 C	5.4 55 1	6.1 - 54 10	13 17	37 1	7.7 1 97 23	1.9 J2 33 32	.8 14. 7 374	7 14.7 373	18.1 463	18.1 462	10.2 262	$\frac{10.2}{262}$	0.4 68 1787 1	$\frac{8.5}{746} \frac{3.}{1}$	$\frac{1}{.57}$ $\frac{31}{14}$	7	10		12		251 4 23 258		2
٠.		1731	55.9 40 1412 10 55.6 40	8 34.2 30 866	479	108	572	359 9	01 !	41 7	48 5	105	524	524	362	362	353 3	351	247	246	305	266	25	257	25	1 - 260	6 - 26	() [(56 H	5.5 1	54 1.	10 4.	12 20	01 2:	8 32	8 374	373	464	461	261	260	792 1	756 1	5 315	2 8	11	380 179 395	41 -	84 10 497 88	4.27 260	2.48	25
2 11	61 15	1739	1413 10 55.6 40	21 861	177	909	569	361 5	09 5	49	55 5	908	525	521	363	363	54 3	53	249	247	308	262	256	256	252	0 10	3 26	1 16	37 10 3.0 (15 1	55 1 6 1	10 4	13 20 7 J · :	8 0 10	50 33 12 13	9 14	7 14 3	18.1	18 1	10.3	262 1	1793 1 o 6 6	746 1	.66 15 6 33		11	386		88	3 4.35 265		
	63.02	1731	1417 10	33 862	479	908	567	358	399	944	49 .	100	526	521	358	363	356 2	347	247	246	300	262	258	1 25	0 249	9 26	4 25	1 1	151 f	1.5	61.	13 1	7 H -	7 9 10	1 1 19	9 11	8 14 3	18.3	18.3	10.3	10.9 7	0.4 6	8.6 3.	5 88	5		386 . 177	99	84	263		
! "	11101	n oo a	1417 10 55.8 4 1414 10	0 110	10 6	3	262 12	1100	Mr Oil	- 0 1	11 0 11	00 0	90 5	11 5	14 9	1 4 4 1	1011	1 ()	0.0	0.0	10 0	1 7 / 2 /	1 10	1 110	1 10	0110	111111	131 6	5 65 (i. 61 -	611.	1 1 11.	7 65 2	8 1 11	14 119	1 14	9114 5	118 4	118.33	101.31	110.35 17	0.5 6:	9.41 135.	.) 3.5			390 .	22.4	88 1	267		
25 "	143. 64.71	1 68.2	55.7 4	1.0 34.1	18.5	35 9 922	22.5 570	14.4	94	7.7	0,3 ;	36.0 914	20.7 519	20.6	14.1 359	362	4.0 1	3.9	249	9.8	12.2	265	259	4 10.	$\frac{1}{1}$ $\frac{10}{25}$	0 10.	$\frac{.5}{7}$ $\frac{10}{26}$	30 10	1.6 6 68 10	67 1	6.1 54 1	11 4	7.5 20 47 20	8.2 10 05 20	5 13 31 33	1 14. 5 384	382	471	18,1	10.8 263	$\frac{10.3}{262}$	0.1 68	761 1.	$\frac{2}{44}$, $\frac{813}{156}$	7		179	43 1	88 89 489	4.45	2.64	-
	142.	a 68.9	56.7 4	1.0 34.1	19.2	36.3	22.4	14.1	5.2	37.4 :	29 5 3	36.0	20.4	20.3	14.1	14.2	2,8	3.8	9,8	9.8	12.0	10.	1 10.	2 10.	0 9,	9 10.	.5 10.	.2 (3,3 (3.6 ¹	6.1	(.C.I.	7.6	8.1.40	3.13	.2 15.	1 15.0	18.5	18.5	10.3	10,3 7	1.7 69	9,8 ¹ 8.	2 33		1	395	95	86	271		143



on or me tric

the state of the s

. 1131 / (.)

14. 11

Hips. 2 860 33.9 3 860 7 33.9 3 864 7 34.0 3C₃ 864 he 7 34.0 38 873 -.8 B4.4 09 879 3.0 34.6 10 881 3.0 34.7 710 882 18.0 34.7

722 884 28.4 34.8 722: 886 28.4 34.8 1723 886 28.4 34.8

723 1 888

714: 882 28.1 34.7

28.4 34.9 726 895 28.5 35.2 729 896 28.7 35.3

731 908 28.7 35.7 738 912 9.0 85.9

738 912 9.0 35.9 741 912 19.2 35.9

9.4 86.2 748 921 9.4 36.2

48 922 9,4 36.8

749 923 9.5 36.3



Anthropometric Study of the Students of Amherst College.

6. TABLE OF HEIGHTS.-1322 MASUREMENTS.

The black figures represent millimeters, kilograms and liters: \mathbf{t}_{led} , inches, pounds and cubic inches.

March, 1892.

			March, 1892.
HEIGHTS	GIRTHS. :: 1	BREADTHS. LENGTHS!	STRENGTHS.
WEIGHT Sternum. Navel. Pubes. Knee. Sitting. Head. Nock. Chest Repose Chest Pull. Belly. Hips.	ett Thigh. ett Thigh. ett Knee. ett Knee. Sight Calf. Eight Calf. Eight Instep. ett Calf. Eight Instep. Eight Eight Ipper Right Ipper Left Ipper Fert	the cent. ceck. pipies. pipies. pipes. pi	nuge. tek. 1) 1) 1) 1) 1) 1) 1) 1) 1) 1
1600 mm. 58.9: 1290 947 797 425 851 559 335 851 881 702 860 500 63.0 in. 118.5 50.8 87.4 81.3 16.7 83.5 22.0 13.2 33.5 84.6 27.7 33.9 19.7	497 341 339 325 323 231 229 275 248 244 241 287 253 248 161) 151 104 413 191 245 313 349 346 480 429 242 241 1660 1610	1.3 126 10 11 130 34 31 470 3.16 2.2
1610 mm. 54.0. 1300 958 800 430 856 561 338 852 882 703 860 501 63.4 in. 118.5 51.2 37.8 81.6 16.9 33.7 22.1 13.4 33.6 84.7 27.7 33.9 19.7	19.5 13.4 13.3 12.8 12.7 9.1 9.0 10.8 9.8 9.6 9.5 9.3 10.0 9.8 6.3 498 341 339 326 324 231 229 277 248 244 241 237 253 248 161	2 5.9 4.1 16.2 7.5 9.6 12.3 13.7 13.6 16.9 16.9 9.5 9.5 65.4 63.4 151 104 416 192 245 313 351 349 434 433 244 243 1690 1620	2.9 278 287 75 68 193 1.3 126 7 10 143 34 31 430 3.21 2.4
1620 mm. 54.1 1300 962 810 439 869 562 340 854 888 703 864 5	19.6 13.4 13.3 12.8 12.7 9.1 9.0 10.9 9.8 9.6 9.5 9.3 10.0 9.8 6.3 498 342 340 333 331 232 230 280 248 244 242 238 253 248 162		3 2.9 278 315 75 68 196
63.8 in. 119.0 51.2 87.9 31.9 17.3 84.2 22.1 13.4 33.6 34.9 27.7 34.0 15 1630 mm. 54.5 1320 966 812 442 870 562 345 857 900 703 864 50	19.6 13.5 13.4 13.1 13.0 9.1 9.0 11.0 9.8 9.6 9.5 9.4 10.0 9.8 6.4	3, 5.9 4.1 16.4 7.6 9.6 12.4 13.9 13.8 17.2 17.1 9.6 9.6 66.5 64.1	6 3.1 278 324 75 68 198
64.2 in. 119.9 52.0 88.0 32.0 17.4 84.3 22.1 13.6 33.7 35.4 27.7 34.0 19.7 1640 mm. 54.7 1330 974 814 448 879 563 345 857 900 708 873 503	19.6 13.5 13.4 13.2 13.1 9.2 9.1 11.0 9.9 9.8 9.5 9.4 10.0 9.8 6.4	3 6.0 4.1 16.5 7.6 9.6 12.4 13.9 13.8 17.2 17.2 9.6 8.6 66.5 65.	
64.6 in. 120.3 52.2 38.4 32.1 17.6 34.5 22.2 13.6 33.7 35.4 27.8 34.4 19.8 1650 mm, 55.5 1340 979 820 448 880 563 346 864 901 709 879 504	498 344 342 336 334 234 232 252 253 249 242 238 254 249 162 19.6 13.5 13.5 13.2 13.1 9.2 9.1 11.1 10.0 9.8 9.5 9.4 10.0 9.8 6.4		
65.0 in. 122.1 52.8 88.5 32.3 17.6 34.6 22.2 13.6 34.0 35.4 28.0 34.6 19.8	500 346 344 387 335 236 233 283 254 250 242 238 255 250 162 19.7 13.6 13.5 13.3 13.2 9.3 9.2 11.1 10.0 9.8 9.5 9.4 10.0 9.8 6.4		0 - 1.3 127 6 10 150 37 34 424 3.44 2.4
1660 mm. 57.3 1350 983 885 450 883 565 347 865 903 710 881 5°° 65.4 in. 127.1 53.2 88.8 33.0 17.7 84.7 22.2 13.7 34.0 55.5 88.0 34.7 1	503 347 345 340 338 236 233 285 254 250 245 241 256 251 162 19.8 13.7 18.6 13.4 13.3 9.3 9.2 11.2 10.0 9.8 9.6 9.5 10.1 9.9 6.4	0 153 107 429 195 248 316 361 356 445 444 252 251 1700 168	0 - 1.2 128 7 11 151 37 34 423 3.50 2.3
1670 mm. 57.9 1350 986 839 454 884 565 348 868 904 710 882 4 65.7 in. 127.3 53.2 88.9 33.1 17.8 84.8 22.2 13.7 34.2 35.5 28.0 34.7 20.6	506 348 346 342 340 237 235 285 254 250 245 241 257 252 163		
1680 mm. 60.1 1360 991 853 460 891 565 348 872 905 714 882 517	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 6.0 4.2 16.9 7.7 9.8 12.5 14.2 14.1 17.5 17.5 9.9 9.9 67.7 66.	
1690 mm. 60.2 1400 1020 862 473 905 566 350 872 909 722 884 517	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		5 2.6 287 850 86 79 216
66.5 in. 132.4 55.1 40.2 34.0 18.6 35.6 22.3 13.8 34.3 35.8 28.4 34.8 20.3 1700 mm. 61.3 1400 1020 1863 474 908 571 1350 876 913 722 886 518	20.2 13.9 13.8 13.6 13.5 9.3 9.2 11.3 10.1 10.0 9.8 9.6 10.3 10.1 6.4	4 6.0 4.2 16.9 7.7 9.9 12.7 14.4 14.3 17.7 17.7 10.0 9.9 68.5 66.	9 2.4 298 363 86 79 220
66.9 in. 134.8 55.1 40.2 34.0 18.7 35.7 22.4 13.8 34.5 35.0 28.4 34.8 20.4 1710 mm. 61.3 1400 1020 863 474 908 571 352 880 916 723 886 519	20.8 13.9 13.9 13.6 13.5 9.8 9.2 11.4 10.1 10 0 9 8 9.6 10.3 10.1 6.5	1 153 108 431 196 253 380 367 364 455 454 256 255 1770 175 4 6.0 4.2 16.9 7.7 10.0 13.0 14.4 14.3 17.9 17.9 10.1 10.0 69.7 67.	
67.3 in. 134.8 55.1 40.2 34.0 18.7 35.7 22.4 13.9 34.6 36.1 28.4 34.8 20.4	516 355 354 347 345 239 237 292 257 253 249 245 262 257 166 20.3 14.0 13.9 13.7 13.6 9.4 9.3 11.5 10.1 10.0 9.8 9.6 10.3 10.1 6.5	4	
1720 mm. 61.7 1410 1020 867 478 910 572 353 887 926 723 888 520 67.7 in. 135.7 55.5 40.2 34.1 18.8 35.8 22.5 13.9 34.8 36.5 28.4 34.9 20.5	517 357 355 347 345 241 239 293 260 258 252 248 263 258 166 20,3 14.0 14.0 13.7 13.6 9.5 9.4 11.5 10.2 10.1 9.9 9.8 10.3 10.1 6.5	4 153 108 432 197 254 332 369 366 460 459 260 259 1780 176 4 6.0 4.2 17.0 7.7 10.0 13.1 14.5 14.4 18.1 18.1 19.2 19.2 70.1 69	0 1.1 138 7 10 164 40 37 482 3.78 2.7
1730 mm. 62.1 1410 1040 870 484 918 572 354 887 930 726 895 521 68.1 in. 136.6 55.5 40.9 34.3 19.0 36.1 22.5 13.9 34.8 36.6 28.5 35.2 20.5	518 360 368 851 349 242 240 295 260 258 252 248 263 258 167	5 153 109 432 198 254 332 369 366 465 464 264 263 1810 177	0 1.3 140 6 10 164 40 37 458 3.90 2.5
1740 mm. 62.5 1420 1050 874: 486 918 572 354 889 931 729 896 522 68.5 in. 137.5 55.9 41.3 34.4 19.1 36.1 22.5 13.9 35.0 36.6 28.7 85.3 20.5	20.4 14.2 14.1 13.8 13.7 9.5 9.4 11.6 10.2 10.1 9.9 9.8 10.3 10.1 6.6 519 361 359 351 349 244 241 296 261 257 254 250 263 258 167	5 154 109 432 198 254 335 371 369 468 467 264 263 1810 177	
1750 mm. 63.9 1430 1050 880 486 918 572 355 889 931 731 908 522	20.4 14.2 14.1 13.8 13.7 9.6 9.5 11.6 10.3 10.1 10.0 9.8 10.3 10.1 6.6 1519 364 361 351 349 244 241 296 261 257 254 250 263 258 167	-5 6.1 4.3 17.0 7.8 10.0 13.2 14.6 14.5 18.4 18.4 10.4 10.3 71.3 69 -5 154 109 433 199 254 335 376 373 468 467 265 264 1810 17	
68.9 in. 140.5 56.3 41.3 34.6 19.1 36.1 22.5 14.0 35.0 36.6 28.7 35.7 20.5 1760 mm. 65.1 1440 1060 886 489 924 573 355 890 931 738 912 522	20.4 14.3 14.2 13.8 13.7 9.6 9.5 11.6 10.3 10.1 10.0 9.8 10 3 10.1 6.6 519 365 363 353 351 245 243 296 260 258 254 250 264 259 168	5 6.1 4.3 17.0 7.9 10.0 13.2 14.8 14.7 18.4 18.4 10.4 10.4 71.3 69	7 2.6 309 368 90 84 240
69.3 in. 56.7 41.7 34.9 19.8 36.4 22.5 14.0 35.0 36.6 29.0 85.9 20.5 1770 mm. 67.8 1450 1060 895 494 925 574 355 890 934 738 912 523	20.4 14.4 14.3 13.9 13 8 9.6 9.6 11.6 10.2 10.1 10.0 9.8 10.4 10.2 6.6	5 6.1 4.8 17.2 7 9 10.0 13.2 15.0 14.9 18.4 18.4 10.4 10.4 71.8 69	.7 2.6 311 370 90 84 245
69.7 in. 57.1 41.7 35.2 19.6 36.4 22.6 14.0 35.0 36.7 29.0 35.9 20.6 1780 mm. 67.8 1450 1070 896: 499 925 575 356 891 936 741 912 523	519 366 364 353 351 245 243 296 260 258 255 251 265 261 168 20,4 14,4 14,3 13,9 13.8 9.6 9.6 11,6 10,2 10,1 10,0 9.9 10,4 10,3 6.6	5 6.1 4.3 17.2 7.9 10.1 13.2 15.0 14.9 18.5 18.5 10.5 10.4 71.3 70	.1 2.9 811 870 90 81 246
70.1 in. 57.1 42.1 35.2 19.7 36.4 22.6 14.0 35.1 36.8 29.2 35.9 20.6	519 366 664 353 351 246, 244 297 261 259 255 251 266 261 168 20.4 14.4 14.3 13.9 13.8 9.7 9.6 11.7 10.3 10.2 10.0 9.9 10.5 10.8 6.6	1 154 109 438 200 256 336 384 381 475 474 267 266 1820 178 6.1 4.3 17.2 7.9 10.1 13.2 15.1 15.0 18.7 18.7 10.5 10.5 71.7 70	
1790 mm. 68.0 1460 1080 899 500 933 576 356 893 936 745 916 523 70.5 in.	519 367 365 354 352 247 245 300 261 259 256 252 267 262 169 20.4 14.4 14.4 13.9 13.9 9.7 9.6 11.8 10.3 10.2 10.1 9.9 10.5 10.3 6.6	1 155 109 438 201 256 237 395 392 480 479 270 269 1850 175	00: 1.2 142 5 9 171 42 40 456 4.18 2.3
1800 mm. 68.2 1470 1090 907 504 934 582 356 894 938 748 921 524 70.9 in. 57.9 42.9 35.7 19.9 36.7 22.9 14.0 35.2 36.9 29.4 36.2 20.6	522 369 367 354 352 247 245 300 261 259 256 252 268 263 170	1 155 109 439 201 256 340 396 893 484 483 273 272 1870 17	90" 1.1 145 5 8 172 43 40 456 4.42 2.2
1810 mm. 68.2 1480 1090 918 517 937 582 356 898 939 748 921 524 71.3 in. 58.3 42.9 36.1 20.3 36.8 22.9 14.0 35.3 37.0 29.4 36.2 20.6	20.5 14.5 14.4 13.9 13.9 9.7 9.6 11.8 10.3 10.2 10.1 9.9 10.5 10.3 6.7 522 369 367 356 354 247 245 300 262 260 256 252 268 263 171	1 156 109 439 205 260 341 396 393 485 484 274 273 1880 178	nt 1.2 147 5. 8 173 43 40 485 4.43 2.4
1820 mm. 68.8 1480 1090 919 519 939 583 356 898 953 748 922 526	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 156 109 440 206 263 341 397 394 486 485 274 273 1890 18:	
71.7 in. 58.8 42.9 36.2 20.4 37.0 23.0 14.0 35.3 37.5 29.4 36.8 20.7 1830 mm. 68.3 1505 1120 921 525 939 583 356 899 956 749 923 529	20.6 14.5 14.4 14.0 18.9 9.7 9.6 11.8 10.3 10.2 10.1 9.0 10.6 10.4 6.7 527 369 367 356 354 247 245 300 264 262 257 253 269 264 172	4. 6.2 4.3 17.3 8.1 10.3 13.4 15.6 15.5 19.1 19.1 10.8 10.7 74.4 71	.7 2.4 324 384 95 88 270
72.0 in. 59.8 44.1 36.8 20.7 37.0 28.0 14.0 35.4 37.6 29.5 36.8 20.8	20.7 14.5 14.4 14.0 13.9 9.7 9.6 11.8 10.4 10.3 10.1 10.0 10.6 10.1 6.8	1 66 109 445 206 263 341 398 395 488 487 276 275 1890 18 1 6,2 4.8 17.5 8,1 10.3 13.4 15.7 15.5 19.2 19.2 10.9 10.8 74.4 72	
•			



Anthropometric Study of the Students of Amherst College.

7. TABLE OF PERCENTAGES.—2230 MEASUREMENTS.

The black figures represent millimeters, kilograms and liters; the red, inches, pounds and cubic inches.

	0 n										===																														
-:		-	HEIGH	TS,										GIR	THS.								1	1			1	BREAD	THS.				LENG	GTHS.			S'	TRENG	THS.		9
PER CENT	WEIGHT	Body.	Navel.	Pubes. Knee.	Sittiog.	Head.	Neck, Chest Repose.	Chest Full.	Belly.	Hips.	Right Thigh.	Right Knee.	Left Knee.	Right Calf.	Left Culf. Right Instep.	Left Instep.	Upper Right Arm Contra't'd	Upper Right Arm,	Upper Left Arm.	Right Elbow. Left Elbow.	Right Forearm	Left Forearm.	Right Wrist	Left Wrist.	Head.	Neck,	Waist.	Hips.	Nipples. Right Shoulder	Left Shoulder Elbow.	Right Elbow Tip.	Leit Eloew Tip.	Left Foot.	Stretch of Arms,	Length.	Lungs. Back.	Dip.	Pul).	Legs. Right Forearm	Left Foreavm.	Fotal.
5	74.3 18 163.7 71	$.9 \mid 59.1$	43.6 30	$egin{array}{c c} 36 & 523 \ .8 & 20.6 \ \hline \end{array}$	$\begin{vmatrix} 954 \\ 37.5 \end{vmatrix}$	$egin{array}{c c} 593 & 3 \ 23.3 & 18 \end{array}$	$egin{array}{c c} 384 & 969 \ 5.1 & 38.1 \ \end{array}$	39.8	32.1 3	37.9 2	$egin{array}{c c} 571 & 50 \ 2.5 & 22 \ \end{array}$	3 15.3	3 388 3 15.3	$\begin{array}{c c} 381 \\ 15.0 \end{array}$	$380 \mid 26 \ 5.0 \mid 10.$	$7 \mid 265 \\ 5 \mid 10.4$	335 1 13.2	$egin{array}{c c} 292 \ 11.5 \ \hline \end{array}$	$egin{array}{c c} 288 & 2 \ 11.3 & 10 \ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c} 0 & 289 \\ 6 & 11.3 \end{array}$	280	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	77	$\begin{bmatrix} 163 & 3 \\ 6.4 & 4 \end{bmatrix}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c} 68 & 281 \\ 3.4 & 11.1 \end{array}$	352 13.9	222 40 8.8 15	$03 \mid 402 \\ .9 \mid 15.8$	494 3 19.4 1	$ \begin{array}{c cccc} \hline 492 & 27 \\ 9.4 & 10. \end{array} $	$9 279 \\ .9 10.9$	$\begin{vmatrix} 1910 & 1 \\ 75.2 & 7 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	16 23 53	$ \begin{array}{c cccccccccccccccccccccccccccccccccc$	0 0	644 4.9 1420 301
10	157.0 71	1 58.3	43.0 36	$\begin{array}{c c} 19 & 512 \\ .1 & 20.2 \end{array}$	943 37.1 2	$\begin{vmatrix} 588 & 3\\ 3.2 & 14 \end{vmatrix}$	$.97 - 949 \ .9 37.3$	$\begin{vmatrix} 992 \\ 39.1 \end{vmatrix}$	$egin{array}{c c} 794 \mid & 31.2 \mid 3 \end{array}$	$\begin{array}{c c} 948 \\ 7.3 \end{array}$	559 5	$\begin{array}{c c} 56 & 386 \\ 9 & 15 & 6 \end{array}$	$\frac{380}{15.0}$	$\begin{bmatrix} 374 \\ 14.7 \end{bmatrix} 1$	371 20 4 6 10	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$0 \mid \begin{array}{c} 327 \\ 12.9 \end{array}$	$\begin{bmatrix} 286 \\ 11.2 \end{bmatrix}$	280 2	269 26	4 281	275	175 1	74	161	116 4	$61 274 \\ 3.1 10.8$	345	217 39	7 395	486	$ \begin{array}{c cccccccccccccccccccccccccccccccccc$		1886 1 74.2 7			12	14 2	19 50	47	594 4. 1310 280
20	149.6 69.	0.9 57.3	$\begin{vmatrix} 1070 & 8 \\ 42.1 & 35 \end{vmatrix}$	$\begin{bmatrix} 499 \\ .3 \end{bmatrix} \begin{bmatrix} 499 \\ 19.6 \end{bmatrix}$	930 36.6 2	$\begin{array}{c c} 581 & 3 \\ 22.8 & 14 \end{array}$	69 925 -6 36.4	$\begin{array}{ c c c }\hline 970 \\ 38.2 \\ \end{array}$	$\begin{bmatrix} 769 \\ 30.3 \end{bmatrix}$	$\begin{array}{c c} 929 & \\ 6.5 & 2 \end{array}$	$\begin{bmatrix} 542 & 5 \\ 1.4 & 21 \end{bmatrix}$	$ \begin{array}{c c} 39 & 373 \\ 2 & 14.7 \end{array} $	$\frac{3 372}{14 7}$	$\frac{364}{14.3}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} 5 & 253 \\ 0 & 9.9 \end{bmatrix}$	$\frac{3 315}{12.4}$	$\begin{bmatrix} 277 \\ 10.9 \end{bmatrix}$	270 2	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9 275	269	171 1	70	158	113 4		338	209 38	88 387	478	1.			. 11	1.7 160 64 259	10	12 19	99 46	43	542 4. 1194 269
30	65.4 177 144.1 69	OU LITUU	1 11/07/1 0	001 1301	32 I II	23 4 4 1 2	660 971	II Moal	1.5.7	U13.51 I	-011 F	301 DAG	1 44 4 4 4 5 1		A = A A =	01 010	01 000		0.01			2	H 14.63		156	111 4	45 261	333	204 3	32 380	172	471 26	66 266	1829 1	769 1	$1.6 \mid 150 \\ 3.52 \mid 331$	8	11 1	84 43	41	507 4.5
40	63.5 173 140.0 68	OO ETSA	1 1040 0	74 L 486 L	91311	57 LL 3	5 /I - 895	$+$ 940 $^{\circ}$	7.105	Onat	~ 15 m	101.074	3 1 A3 / L S 1	OMO	OHAL OF	41 0 4 5		0.01	D H O 1 1			1	- 001 -					329	200 3	77 875	6 466	465 26	83 263	1808 1	750 1	1.5 149	1	10 1	75 41	39	$\begin{array}{c cccc} 1117 & 257 \\ 479 & 4.6 \\ 2000 & 240 \\ \end{array}$
50	61.6 172 135.8 67.																			250 - 24	7 262	256	165 1	63	153	108 4	i	325	196 3'	3 371	461	459 26	60 260	1789 1	739 1	$\frac{1.4}{1.4}$])	9 10	69 + 39	37	1056 24 <i>l</i> 153 3.3
40	59.9 171 132.0 67.	10 1000	1019 84 40.1 33	24 400	897 H	5041 - 3	48' - 870	0.9137	7181	889	2021 -	111 0 = 0	0 4 4	0.41	arol ar	0 000	$0 \mid 289$	253	248 5	249 24	$rac{ 10.3 }{2 259 }$	252	163 1	61	$\begin{array}{c c} 6.0 & 4 \\ \hline 152 & \end{array}$	$\frac{4.3}{107} \frac{17}{4}$	$27 \mid 249$	321	192 3	69 367	7 456	454 ²⁵	$57 \mid 257$	1769 1	723 1	$\frac{3.08}{1.2} \frac{300}{130}$	0 4	8 1.	57 37	35	999 23 431 3.
30	57.8 169 127.4 66.	92 168U	$\square \cup \cup \cup A \sqcup S_4$	-2.14611	888 117	$560 \pm 2i$	191 950	000	CO 4 1 1	071) "	100 11	3 .3 44	1				11.4			$\begin{array}{c c} .8 & 9.5 \\ 44 & 23. \end{array}$		0.0	$\begin{array}{c c} 6.4 & 6 \\ 1.61 & 1 \end{array}$		-	ī	21 245	317	189 36	64 363	i i	449 25	4 254	1749 13	709 1	$\frac{.64 + 28}{1.1 + 124}$	7 3-		49 35	33	950 226 406 3.
20	127.4 66. 55.9 167 123.2 65.	(+ 11365	-3002 ± 82	9 1 2 5 2 1	879 H #	5561.99	201 044	1 001	COOL	0.50							$\begin{array}{ c c c }\hline 11.1\\\hline 275\\\hline \end{array}$	$\begin{array}{ c c }\hline 9.7 \\ \hline 242 \end{array}$	$\frac{9.5 \mid 9}{237 \mid 2}$	$\frac{0.6 + 9.4}{39 + 234}$	1 10.0 1 250	9.8	6.3 6	5.3 58	5.9 4 149 1	103 4	$ \begin{array}{c c} 3.6 & 9.7 \\ \hline 13 & 240 \end{array} $	313	184 35	$\overline{69} \overline{357}$	445	44 25	1 251	1725 10	387 1	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	$6 \begin{vmatrix} 3 \\ 13 \end{vmatrix}$	$\frac{28 \mid 77}{39 \mid 33}$		892 217 374 3.3
10	123.2 65. 53.4 164 117.7 64.	17 1339	970 81	$\frac{2}{2}$	366 5	550 39	0 33.2	01.1 2	61 10	342	$egin{array}{c c} 9.2 & 19 \ \hline 474 & 47 \ \hline \end{array}$	$\begin{array}{c c} 0 & 13.5 \\ \hline 0 & 335 \end{array}$	13.5	$\frac{12.9}{320}$	$ \begin{array}{c cccc} 2.9 & 9. \\ 320 & 22 \end{array} $	$\begin{array}{c c} 1 & 9.1 \\ \hline 9 & 228 \end{array}$	10.8	$\begin{vmatrix} 9.5 \\ 234 \end{vmatrix}$	$9.4 \mid 9$	$\frac{0.4 + 9.2}{33 + 229}$	$\frac{2}{9.8}$	9.5	(6.3 6 1)56 13	$\frac{3.2}{54}$	$\frac{5.9}{147} 1$	$\begin{array}{c cccc} 4.1 & 10 \\ 101 & 40 \end{array}$	$\begin{array}{c c} 0.3 & 9.5 \\ 02 & 235 \end{array}$	1			17.5					$\begin{array}{c c} .20 & 258 \\ 0.8 & 104 \end{array}$	8 1	4 1:	$\frac{306}{24} = \frac{72}{30}$		825 206 339 3.
5	51.0 162 112.4 64.	25 1319	00.2	$\frac{5}{5} + \frac{432}{1}$	853 5	$\frac{1.0 + 13}{545 + 32}$	$\frac{0002.4}{805}$	843	664 3	3.2 . [829] .	$\frac{8.7}{163} \frac{18}{463}$	$\frac{5 13.2}{9 329}$	330	$\begin{array}{c c} 12.6 & 1 \\ \hline 314 & \\ \end{array}$	$ \begin{array}{c cccc} 2.6 & 9. \\ 313 & 22 \end{array} $	$0 \mid 9.0$	$\begin{array}{c c} 10.4 \\ \hline 258 \end{array}$			$egin{array}{ c c c c c c c c c c c c c c c c c c c$	1 1	230		51	- '	99 3	$ \begin{array}{c c} \hline 6.8 & 9.3 \\ \hline 93 & 230 \\ \end{array} $	301	I73 34	5 343	428	427 24	2 241	10 m = 10 a	637 0	$\begin{array}{c c} 76 & 229 \\ \hline 0.7 & 99 \end{array}$	0	3 1	12 28	26	748 193 309 2.9
	R H					1.07 12	.0 01.7	00.2	411.1 3	2.6].[8.2 18	0.0[12.9]	13.0	12.3 1	2.3 8.	8 8.8	10.1	9,0	8.7	9.0 8.8	8 9.4	9.1	6.0	5.9	$5.7 \mid 3$	8.9 19	5.5 9.1	11.8	6.8 12	3.6 13.	5 16.8	16.8 9.	5 9.4	65.7 [64	.5	$\frac{54}{218}$		2	247 61	.7 57.3	681 178





